

Energy output of solar collectors

Higher Education Package for Nearly Zero Energy and Smart Building Design

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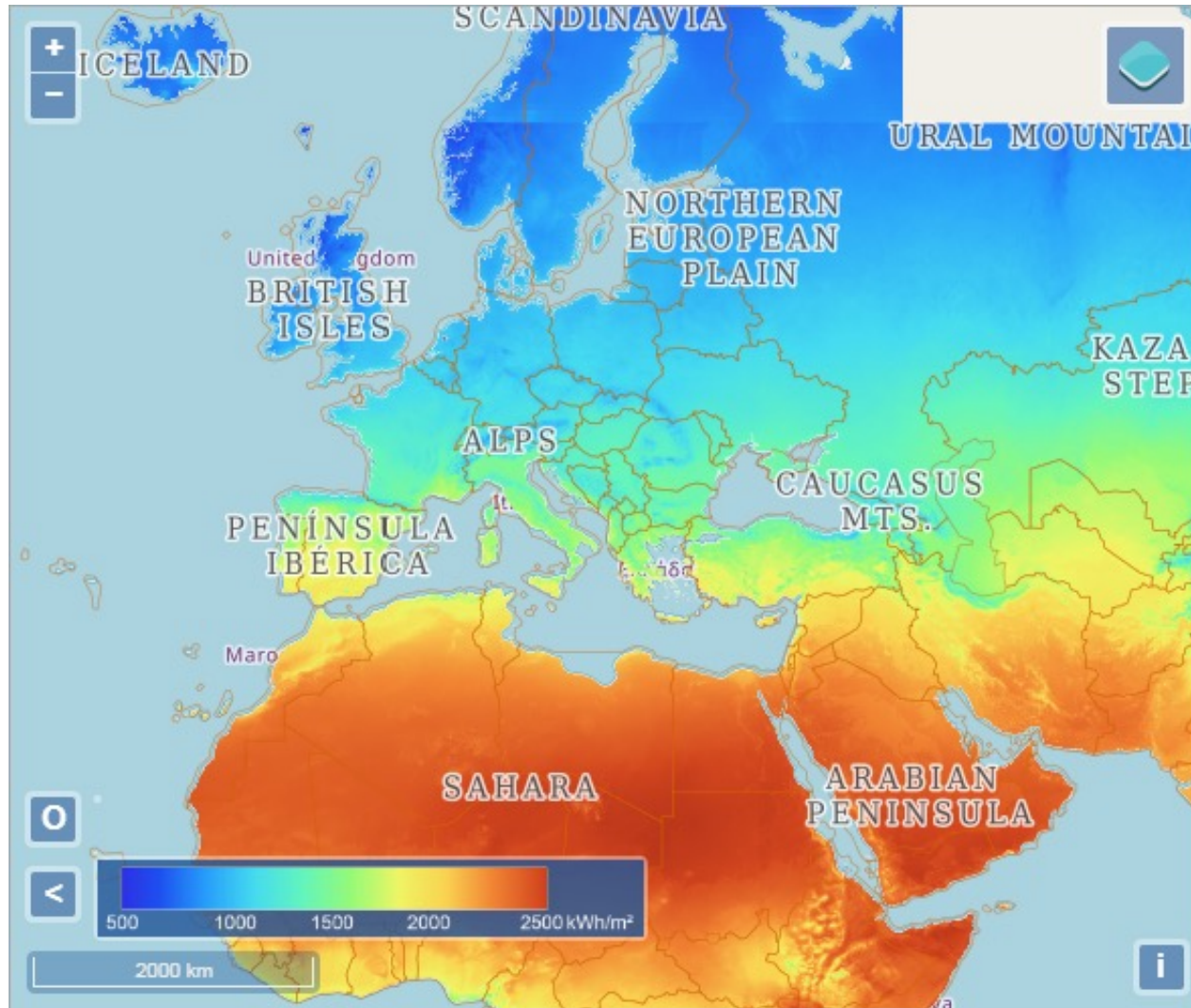


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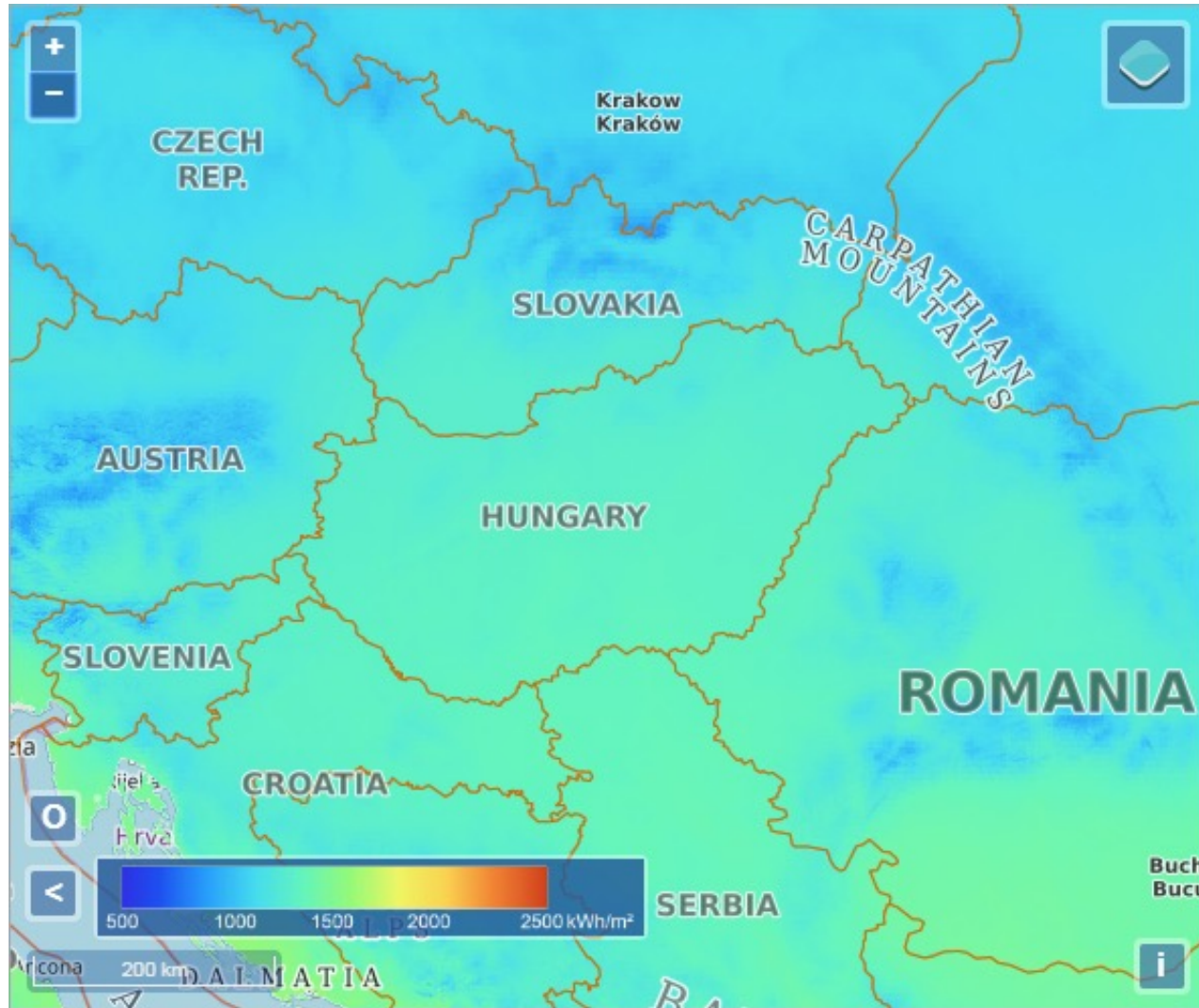


Available solar radiation



Source: http://re.jrc.ec.europa.eu/pvg_tools/en/tools.html#PVP

Available solar radiation



Source: http://re.jrc.ec.europa.eu/pvg_tools/en/tools.html#PVP

Energy output of solar collectors

Meteorological data (yearly, monthly, daily, hourly)

- Solar radiation
- External temperature

Solar collector type

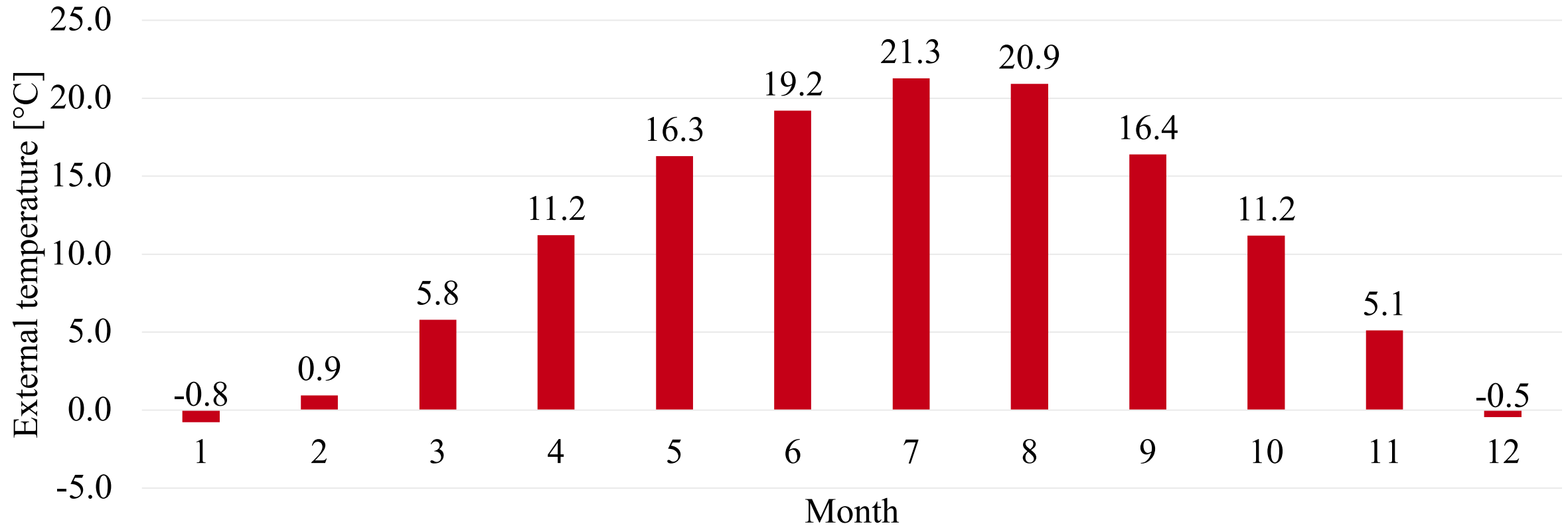
Available roof space, building characteristics

- Roof – orientation, tilt angle

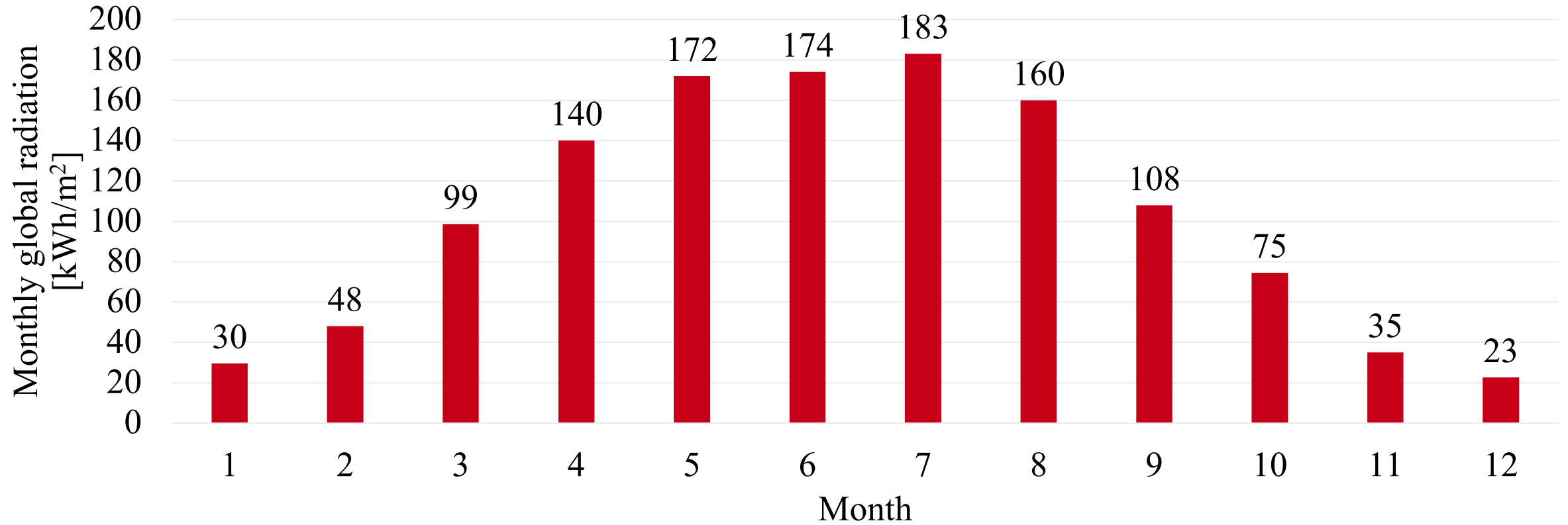
Demand side

- DHW production
- Pool heating
- Space heating
- Other

Meteorological data



Meteorological data



Solar collectors

Type

- Flat-plate collectors
- Vacuum tube collectors

Typical parameters ([Solar Keymark database](#))

- Optic efficiency: η_0
- Temperature dependence coefficients: a_1, a_2
- Dependence on the incident angle of solar radiation: $K_{dir}(50^\circ)$

Solar collector datasheet



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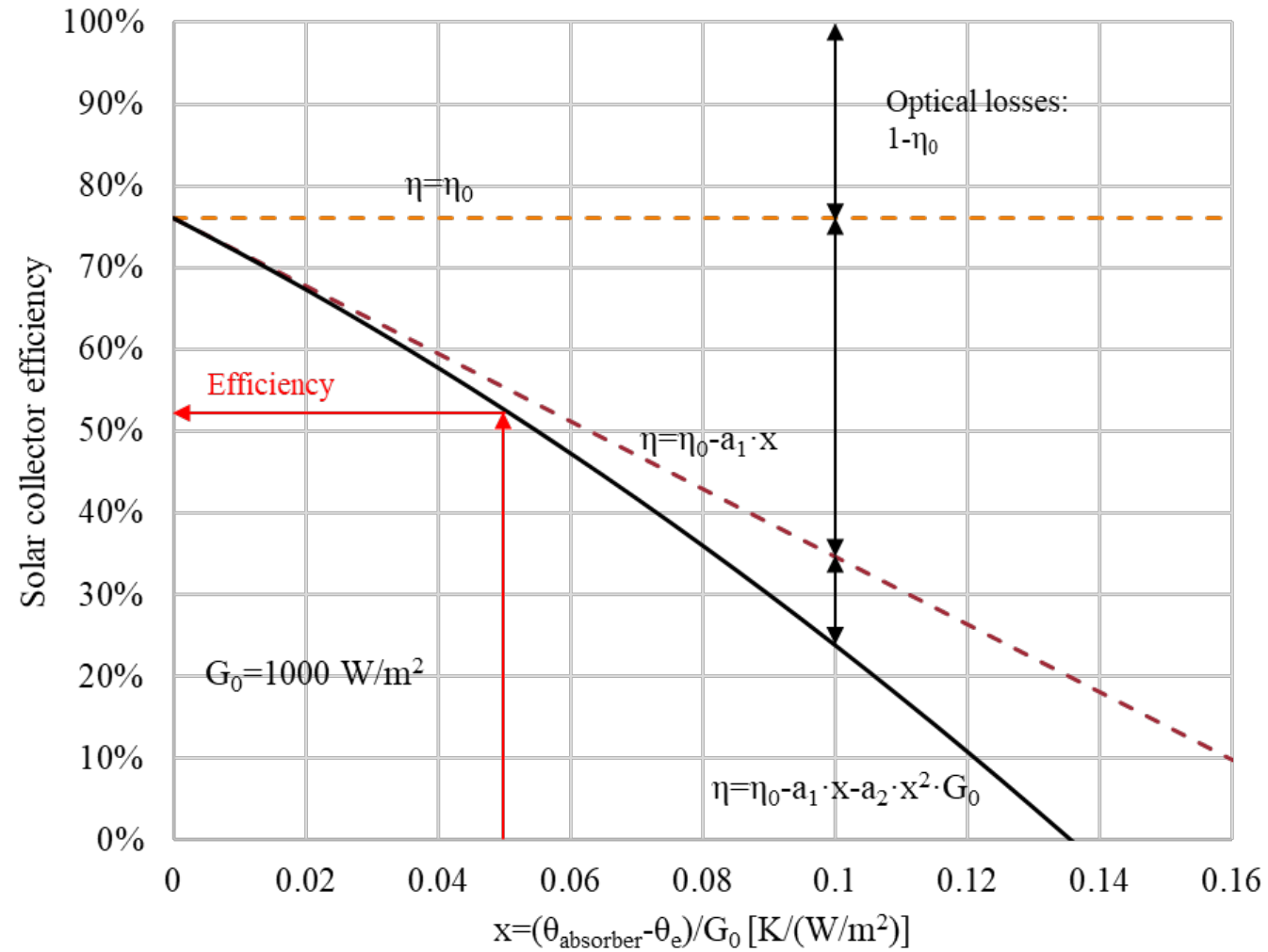
Annex to Solar Keymark Certificate - Summary of EN ISO 9806:2013 Test Results		Licence Number TSU 001-16/D	
Date issued 2016-10-03		Issued by TSU Piešťany, s.p.	
Licence holder ELVOSOLAR a.s.		Country Slovak republic	
Brand (optional)		Web www.elvosolar.sk	
Street, Number Arétovej 22, P.O. BOX 108		E-mail ancic@elvosolar.sk	
Postcode, City SK-841 01 Bratislava		Tel +421 905609462	
Collector Type Flat plate collector, glazed			
Collector name ELVOSOLAR TS300-2.03		Power output per collector G _b = 850 W/m ² , G _d = 150 W/m ² θ _m - θ _a	
Area (A ₀)	2.03 m ²	0 K	10 K
Length	2.008 mm	30 K	50 K
Width	1.008 mm	70 K	90 K
Height	75 mm	W	W
		1.445	1.375
		1.234	1.074
		899	708
Data required for CDR (EU) No 812/2013 - Reference Area A_{sol}			
Zero-loss efficiency (η ₀)	0,712	--	n
First-order coefficient (a ₁)	3,18	W/(m ² K)	Water-Glycole
Second-order coefficient (a ₂)	0,010	W/(m ² K ²)	No
Incidence angle modifier IAM (50°)	0,95	--	No
Energy Labelling Information			
Reference Area, A _{ref} (m ²)	2,03	Data required for CDR (EU) No 811/2013 - Reference Area A _{ref}	Collector efficiency (η _{ref})
			57 %
Remark: Collector efficiency (η _{ref}) is defined in CDR (EU) No 811/2013 as collector efficiency of the solar collector at a temperature difference between the solar collector and the surrounding air of 40 K and a global solar irradiance of 1000 W/m ² , expressed in % and rounded to the nearest integer. Deviating from the regulation η _{ref} is based on reference area (A _{ref}) which is aperture area for values according to EN 12975-2 or gross area for ISO 9806:2013.			
Data required for CDR (EU) No 812/2013 - Reference Area A_{ref}			
Zero-loss efficiency (η ₀)	0,712	--	--
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Incidence angle modifier IAM (50°)	0,95	--	--
Remark: The data given in this section are related to collector reference area (A _{ref}) which is aperture area for values according to EN 12975-2 or gross area for ISO 9806. Consistent data sets for either aperture or gross area can be used in calculations like in the regulation 811 and 812 and simulation programs.			
Testing laboratory Technický skúšobný ústav Piešťany, s.p.		http://www.tsu.sk	
Test report(s) 120700004/1/P(D5) 110700001/1/PQ(D5)		Dated 4.3.2016 4.3.2016	
Comments of testing laboratory Performance parameters - complete re-evaluation of the test data of the previous test (according to EN 12975-2:2006) taking into account gross area.		Datasheet version: 3.01, 2016-03-01	
Technický skúšobný ústav Piešťany, s.p. Address: Krajná cesta 2020/9, 02101 Piešťany, Slovak Republic Phone: +421 33 79 57 111, Fax: +421 33 77 23 716, E-mail: sv@tsu.sk, web: www.tsu.eu			

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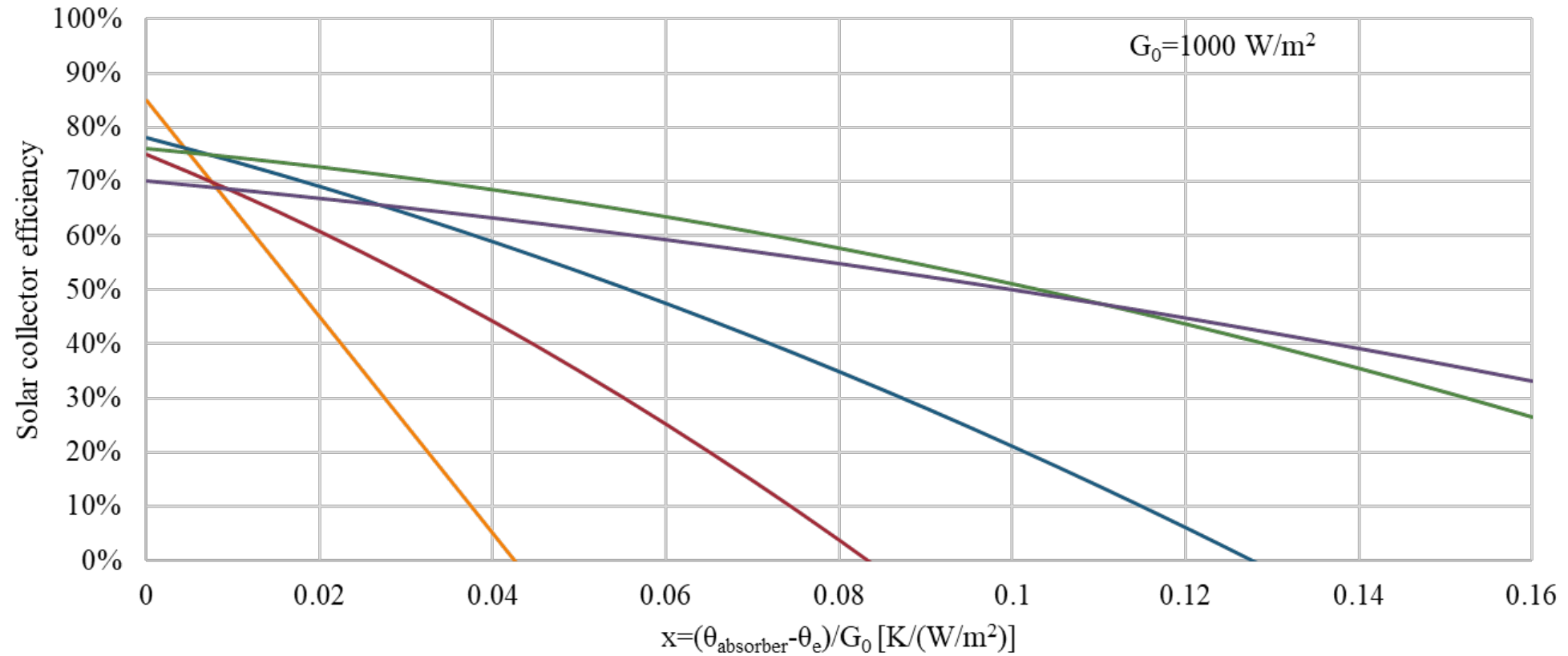
Annex to Solar Keymark Certificate		Licence Number TSU 001-16/D	
Supplementary Information		Issued 2016-10-03	
Annual collector output in kWh/collector at mean fluid temperature θ _m , based on ISO 9806:2013 test results			
Collector name	Standard Locations	Athens	Davos
		Stockholm	Würzburg
		25°C 50°C 75°C	25°C 50°C 75°C
ELVOSOLAR TS300-2.03		2.335 1.707 1.164	1.793 1.277 843 1.319 888 763 1.432 961 599
Annual output per m ² gross area			
		1.130 841 573	883 629 415 650 437 277 705 474 295
Fixed or tracking collector			
Fixed (slope = latitude - 13°, rounded to nearest 5°)			
Annual irradiation on collector plane		1765 kWh/m ²	1714 kWh/m ²
Mean annual ambient air temperature		18,5°C	3,2°C
Collector orientation or tracking mode		South, 23°	South, 30°
		South, 43°	South, 33°
Remark: The calculation of the annual collector output is based on local Ver. 3.01 (March 2016). A detailed description is available in the datasheet.			
Data required for CDR (EU) No 812/2013 - Reference Area A_{sol}			
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Solar collector efficiency



Solar collector efficiency



- Unglazed flat-plate collector
- Glazed flat-plate collector without selective coating
- Glazed flat-plate collector with selective coating
- Vacuum flat-plate collector
- Vacuum tube collector

Demand side

DHW production

- Net DHW demand (usually yearly)
- Distribution and storage losses (usually yearly)

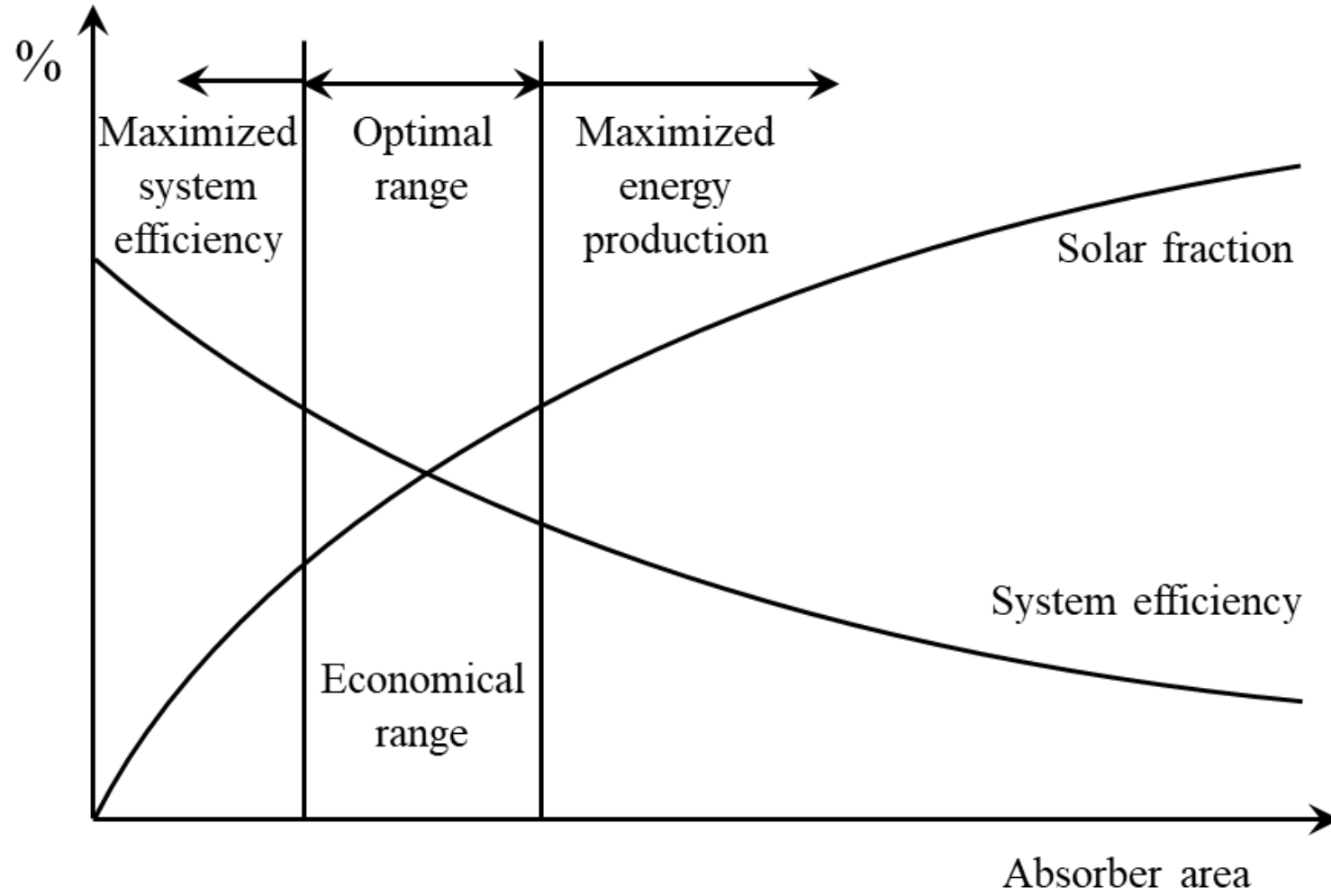
Space heating

- Net heating demand (seasonal)
- Distribution and storage losses (seasonal)

Pool heating

Other

System size

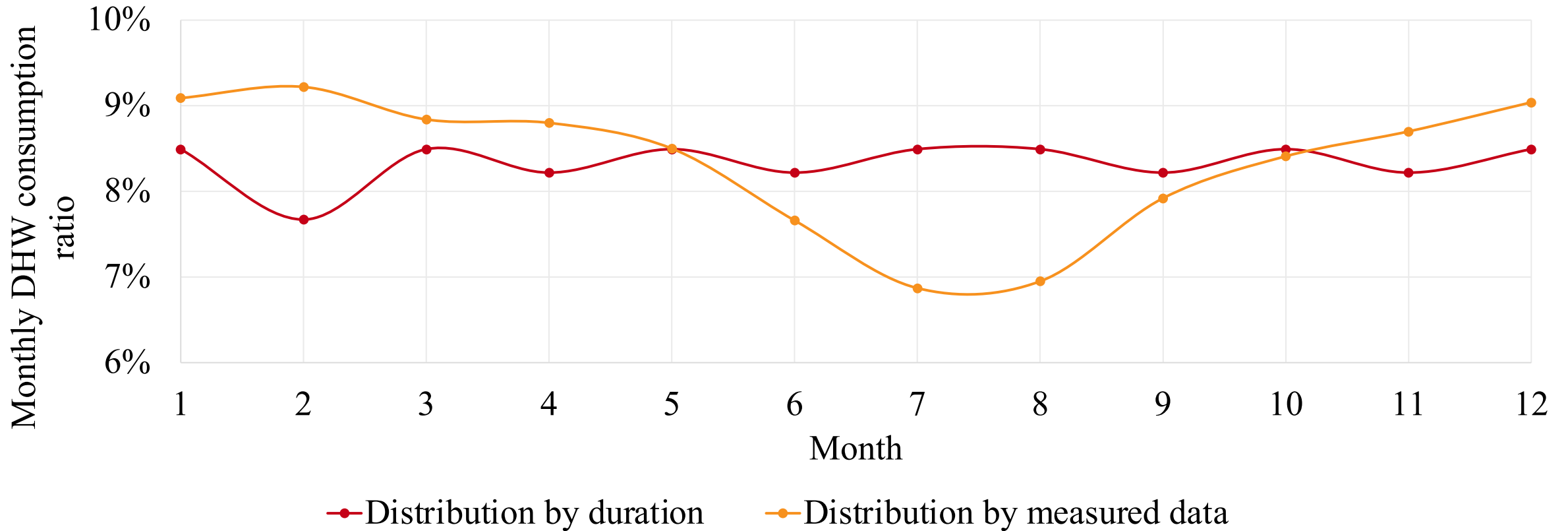


Solar collector production: monthly method

Input parameters

- Collector parameters, η_0 , a_1 , a_2 , $K_{dir}(50^\circ)$, $area$
- Monthly incoming radiation, $Q_{s,i}$
- Monthly DHW system energy demand, $Q_{demand,i}$
- Monthly outdoor temperature, $t_{e,i}$
- Reference temperature for the solar collector, t_{ref}
- DHW temperature, t_{DHW}
- Cold water temperature, t_{CW}
- Solar collector heat removal factor, FR
- Solar collector flow rate, FR'/FR
- DHW storage tank size, V_t

Monthly DHW demand



Solar collector production: monthly method

$$\frac{X_{c1}}{X} = \frac{11,6 + 1,18 \cdot t_{HMV} + 3,86 \cdot t_{v\acute{i}z} - 2,32 \cdot t_{e,i}}{t_{ref} - t_{e,i}}$$

$$\frac{X_{c2}}{X} = \left(\frac{V_{t,a}}{V_{t,opt}} \right)^{-0,25} = \left(\frac{0,7 \cdot V_t}{0,075 \cdot A_{koll}} \right)^{-0,25}$$

$$X = \left(FR \cdot a_1 + FR \cdot a_2 \cdot (t_{HMV} - t_{e,i}) \right) \cdot \frac{FR'}{FR} \cdot (t_{ref} - t_{e,i}) \cdot \tau_m \cdot \frac{A_{koll}}{Q_{ig\acute{e}ny,i}} \cdot \frac{1}{1000}$$

Solar collector production: monthly method

$$X_c = X \cdot \frac{X_{c1}}{X} \cdot \frac{X_{c2}}{X}$$

$$Y = \eta_0 \cdot Q_{s,i} \cdot \frac{FR'}{FR} \cdot K_{dir}(50^\circ) \cdot \frac{A_{koll}}{Q_{igény,i}}$$

$$f_i = \min(1,029 \cdot Y - 0,065 \cdot X_c - 0,245 \cdot Y^2 + 0,0018 \cdot X_c^2 + 0,0215 \cdot Y^3; 1)$$

$$Q_{koll,i} = f_i \cdot Q_{HMV,tot,i}$$

Monthly method – single family house

Final energy demand of DHW system:

$$Q_{DHW} = q_{DHW} \cdot \left(1 + \frac{q_{DHW,d}}{100} + \frac{q_{DHW,s}}{100} \right) \cdot C_k \cdot \alpha_k \cdot A_N$$

Net DHW demand ($A_N=133 \text{ m}^2$)

Above 80 m^2 : $15 \text{ kWh/m}^2\text{year}$

Building type	Net DHW demand $q_{DHW} [\text{kWh/m}^2/\text{year}]$
Residential	30
Office	9
Education	7

$$q_{DHW} = \frac{(80 \cdot 30 + 53 \cdot 15)}{133} = 24.0 \text{ kWh}/(\text{m}^2\text{year})$$

DHW system

Condensing boiler: $C_k = 1.16$

Distribution losses: $q_{DHW,d} = 13\%$

Storage losses: $q_{SHW,s} = 23.4\%$

Solar collector system

- orientation, tilt angle: South, 30°

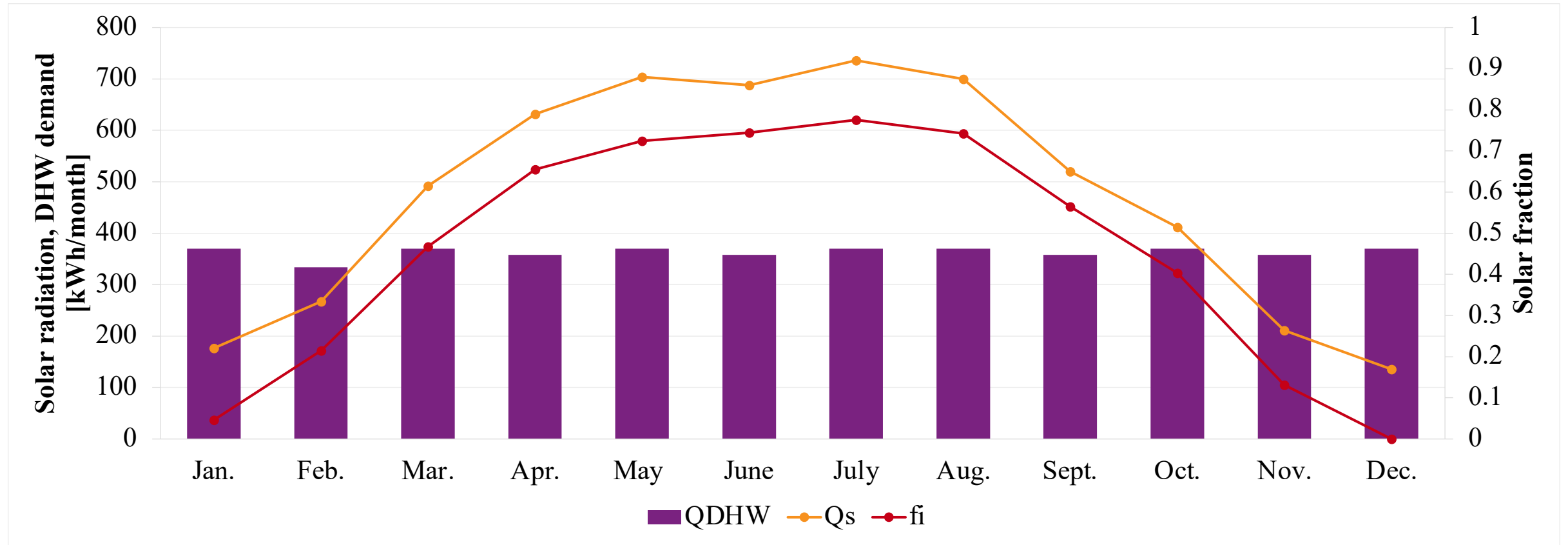
η_0	a_1	a_2	$K_{\text{dir}(50^\circ)}$	FR	FR'/FR	t_{ref}	t_h	t_{HMV}	A_{koll}	V_t
0.79	3.79	0.01	0.92	0.95	0.8	100	10.6	50	4	0.2
[1]	[W/(m ² K)]	[W/(m ² K ²)]	[1]	[1]	[1]	[°C]	[°C]	[°C]	[m ²]	[m ³]

DHW system

Delivered energy demand

$$Q_{DHW} = q_{DHW} \cdot \left(1 + \frac{q_{DHW,d}}{100} + \frac{q_{DHW,s}}{100}\right) \cdot A_N = 24.0 \cdot \left(1 + \frac{13}{100} + \frac{23.4}{100}\right) \cdot 133 = 4354 \frac{\text{kWh}}{\text{year}}$$

Solar collector output



Yearly solar fraction: 45.7%; Yearly DHW production: 1991 kWh

Simplified seasonal method

Limitations for application:

- Only residential DHW demand is covered by the solar collector system.
- The storage is at least 50 l/m² per solar collector area.

Simplified method

Determination of maximal collector production:

- Solar collector type (flat-plate/vacuum tube collector)
- Gross solar collector area
- Reference system area
- Storage and distribution

Reduction factor

Calculation of the solar fraction

DHW system

Condensing boiler: $C_k = 1.16$

Distribution losses: $q_{DHW,d} = 13\%$

Storage losses: $q_{DHW,s} = 23.4\%$

Solar collector system

- Flat-plate collector
- 4 m² gross collector area
- orientation, tilt angle: South, 30°

Maximal collector performance – Flat-plate collector

		Reference system area [m ²]														
		40	50	60	70	80	90	100	110	120	130	140	150	200	250	300
Gross collector area [m ²]	1,5	725	779	817	845	867	884	898	908	917	924	930	936	957	971	980
	2	844	944	1006	1053	1089	1119	1142	1160	1175	1187	1198	1207	1245	1268	1284
	2,5	911	1054	1159	1230	1283	1326	1362	1388	1411	1430	1446	1461	1517	1553	1578
	3	963	1123	1265	1373	1451	1510	1558	1595	1626	1653	1676	1696	1775	1826	1861
	4	1036	1224	1395	1547	1687	1796	1888	1948	1999	2043	2081	2115	2250	2337	2397
	5	1089	1295	1485	1661	1822	1971	2109	2206	2296	2367	2423	2472	2672	2803	2893
	6	1138	1349	1554	1745	1925	2093	2247	2377	2499	2599	2686	2765	3046	3227	3352
	7	1184	1398	1608	1813	2005	2187	2361	2502	2634	2758	2875	2979	3374	3610	3775
	8	1231	1445	1658	1868	2072	2264	2448	2605	2750	2883	3008	3126	3645	3956	4165
	10	1291	1539	1752	1968	2178	2387	2590	2762	2924	3077	3223	3360	4014	4518	4848

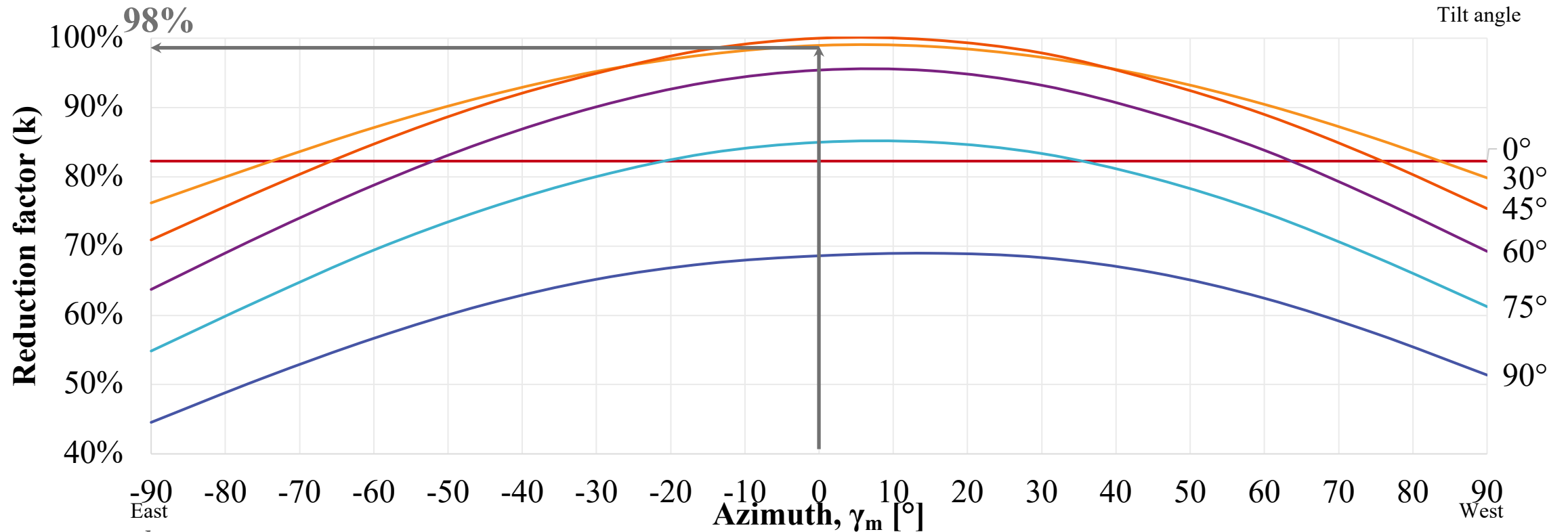
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Above 80 m^2 : $15 \text{ kWh/m}^2\text{year}$

Building type	Net DHW demand $q_{DHW} [\text{kWh/m}^2/\text{year}]$
Residential	30
Office	9
Education	7

$$q_{DHW} = \frac{(80 \cdot 30 + 53 \cdot 15)}{133} = 24.0 \text{ kWh}/(\text{m}^2\text{year})$$

Reduction factor for solar collectors



$$k = (9.88 \cdot 10^{-9} \cdot \alpha_m^2 - 1.18 \cdot 10^{-6} \cdot \alpha_m) \cdot \gamma_m^2 + (-4.99 \cdot 10^{-8} \cdot \alpha_m^2 + 9.25 \cdot 10^{-6} \cdot \alpha_m) \cdot \gamma_m + (-1.17 \cdot 10^{-4} \cdot \alpha_m^2 + 9.11 \cdot 10^{-3} \cdot \alpha_m + 0.821)$$

Solar fraction

$$q_{coll} = \frac{Q_{coll,max} \cdot k}{A_N} = \frac{2043 \cdot 0.98}{133} = \mathbf{15.05 \text{ kWh}/(\text{m}^2\text{year})}$$

$$\alpha_{coll} = \frac{q_{coll}}{q_{DHW} \cdot \left(1 + \frac{q_{DHW,d}}{100} + \frac{q_{DHW,s}}{100}\right)} =$$
$$\frac{15.05}{24.0 \cdot \left(1 + \frac{13}{100} + \frac{23.4}{100}\right)} = 0.460$$

Thank you very much for your attention!

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